

## A Heat Transfer Problem of Viscous Liquid in Porous Media

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**Abstract:** Steady flow of a viscous fluid of finite depth in a porous medium over a fixed horizontal, impermeable bottom is considered in this paper. Exact solutions of Momentum and Energy equations are obtained when the temperatures on the fixed bottom and on the free surface are prescribed. Velocity, Mean velocity, Temperature and Mean Temperature in the flow region have been obtained. The cases of large and small values of porosity coefficient have been obtained as limiting cases. The results are illustrated graphically.

**Keywords:** Viscous fluid, Velocity, Mean Velocity, Temperature, Mean Temperature

### 1. INTRODUCTION

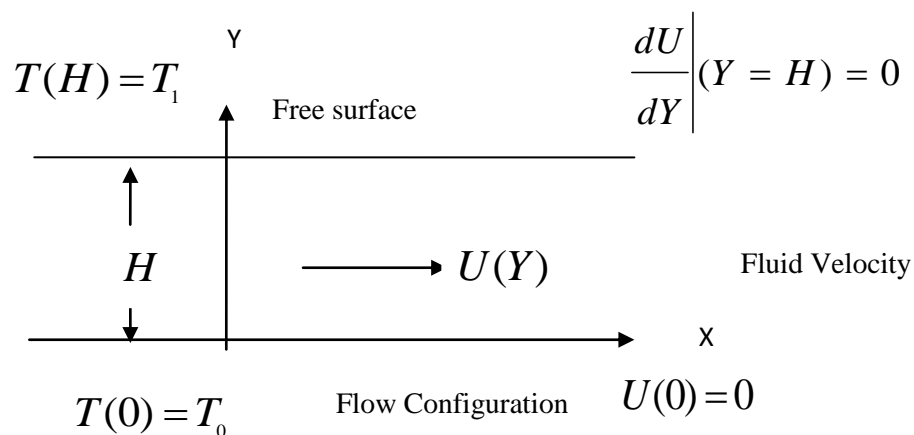
Forced convective flows through porous and non porous channels for a variety of geometries was examined by Raghava Charyulu [1] and Satyanarayana Raju [2]. Md.Ameenuddin and N.Ch.Pattabhi Ramacharyulu [3] studied steady flow of a second order slightly viscous fluid through a porous medium between two horizontal permeable plates in relative motion in the year 2011. Jaweed Ameen[4] studied some investigations on fluid flows through generalized porous media. Raptis et.al [5] examined an oscillary flow through a porous medium in the presence of free convective flow.

In this paper the convective flow of a viscous liquid of viscosity  $\mu$  and of finite depth  $H$  through a porous medium of porosity coefficient 'k\*' over a fixed impermeable bottom is investigated. The flow is generated by a constant pressure gradient parallel to the fixed bottom plate. The momentum equation considered is the generalized Darcy's law proposed by Yama Moto and Iwamura [6] which takes into account the convective acceleration and the Newtonian viscous stresses in addition to the classical Darcy force. The basic equations of momentum and energy are solved to give exact expressions for velocity and temperature distributions. Employing, the flow rate, mean velocity, mean temperature, mean mixed temperature and the nusselt numbers at the fluid boundaries have been obtained and illustrated graphically.

The cases of 1. high porosity and 2. low porosity are also discussed.

### 2. MATHEMATICAL FORMULATION

Consider the steady forced convective flow of a viscous liquid through a porous medium of viscosity coefficient  $\mu$  and of finite depth ( $H$ ) over a fixed horizontal impermeable bottom. The flow is generated by a constant horizontal pressure gradient parallel to the bottom. Further the bottom is kept at a constant temperature  $T_0$  and the free surface is exposed to atmospheric temperature  $T_1$ .



With reference to a rectangular Cartesian co-ordinates system with the origin 'O' on the bottom, X-axis in the flow direction (that is parallel to the applied pressure gradient). The Y-axis vertically upwards, the bottom is represented as Y=0 and the free surface as Y=H. Let the flow be characterized by a velocity  $U = (U(Y), 0, 0)$ . This choice of velocity evidently satisfies the continuity equation  $\nabla \cdot U = 0$  where U is the fluid velocity vector. Further let T(Y) denotes the temperature distribution.

### 3. BASIC EQUATIONS

Let the convective flow be calculated by the velocity field  $U = (U(Y), 0, 0)$  and the temperature T(Y). This choice of the velocity satisfies the continuity equation  $\nabla \cdot U = 0$  [1]

The Momentum Equation is

$$-\frac{\partial P}{\partial X} + \mu \frac{d^2 U}{dY^2} - \mu \frac{U}{k^*} = 0 \quad [2]$$

and the Energy Equation is

$$\rho c U \frac{\partial T}{\partial X} = K \frac{d^2 T}{dY^2} + \mu \left( \frac{dU}{dY} \right)^2 \quad [3]$$

In the above equations  $\rho$  is the fluid density,  $k^*$  the coefficient of porosity of the medium, c is the specific heat, K the thermal conductivity of the fluid and P the fluid pressure.

#### Boundary Conditions:

Since the bottom is fixed,  $U(0) = 0$  [4a]

At the free surface shear stress vanishes

$$\mu \frac{dU}{dY} = 0 \text{ at } Y=H. \quad [4b]$$

Also  $T(0) = T_0$  [5a] and  $T(H) = T_1$  [5b]

where  $T_0$  is the bottom temperature and  $T_1$  is the atmosphere temperature.

In terms of the non-dimensional variables defined as:

$$Y = ay; \quad X = ax; \quad H = ah; \quad U = \frac{\mu u}{\rho a^2}; \quad P = \frac{\mu^2 p}{\rho a^2}; \quad T = T_0 + (T_1 - T_0)\theta; \quad Pr = \frac{\mu c}{k}; \quad k^* = \frac{a^2}{\alpha^2};$$

$$E = \frac{\mu^3}{\rho^2 a^2 K (T_1 - T_0)}; \quad -\frac{\partial P}{\partial X} = \frac{\mu^2 c_1}{\rho a^3} \left( c_1 = -\frac{\partial p}{\partial x} \right) \text{ and } \frac{\partial T}{\partial X} = \frac{(T_1 - T_0)}{a} c_2$$

$$\text{where } c_2 = \frac{\partial \theta}{\partial x} \quad [6]$$

where ‘a’ is some standard length, the basic field equations (2) , (3) can be rewritten as follows:

Momentum Equation:

$$\frac{d^2 u}{dy^2} - \alpha^2 u = -c_1$$

[7] and

Energy Equation:

$$\frac{d^2 \theta}{dy^2} = Pr c_2 u - E \left( \frac{du}{dy} \right)^2 \quad [8]$$

together with the boundary conditions

$$\text{For the velocity } u(0) = 0 \text{ and } \frac{du}{dy} = 0 \text{ at } y=h \quad [9]$$

$$\text{and for the temperature } \theta(0) = 0 \text{ and } \theta(h) = 1 \quad [10]$$

The momentum equation together with the related boundary conditions yield the velocity distribution:

$$u(y) = \frac{c_1}{\alpha^2} \left( 1 - \frac{\cosh \alpha(h-y)}{\cosh \alpha h} \right) \quad [11]$$

The energy equation satisfying the boundary conditions yields the temperature distribution:

$$\begin{aligned} \theta(y) = & \frac{y}{h} + \frac{Pr c_1 c_2}{\alpha^2} \left[ \frac{(h-y)}{h \alpha^2} - \frac{y(h-y)}{2} + \frac{1}{\alpha^2 \cosh \alpha h} \left( \frac{y}{h} - \cosh \alpha(h-y) \right) \right] + \\ & \frac{Ec_1^2}{2\alpha^2 \cosh^2 \alpha h} \left[ \frac{(h-y) \cosh(2\alpha h)}{4\alpha^2 h} - \frac{y(h-y)}{2} + \frac{1}{4\alpha^2} \left( \frac{y}{h} - \cosh 2\alpha(h-y) \right) \right] \end{aligned} \quad [12]$$

The flow rate in the non-dimensional form is

$$q = \int_0^h u(y) dy = \frac{c_1}{\alpha^2} \left( h - \frac{\tanh \alpha h}{\alpha} \right)$$

The mean velocity in the non-dimensional form is

$$\frac{1}{h} \int_0^h u(y) dy = \frac{c_1}{h \alpha^2} \left( h - \frac{\tanh \alpha h}{\alpha} \right) \quad [13]$$

Further the mean temperature in non-dimensional form is given by

$$\bar{\theta} = \frac{1}{h} \int_0^h \theta dy$$

$$= \frac{1}{2} + \frac{P_r c_1 c_2}{\alpha^2} \left( \frac{-h^2}{12} + \frac{1}{2\alpha^2} + \frac{1}{2\alpha^2 \cosh ah} - \frac{\tanh ah}{h\alpha^3} \right) - \frac{Ec_1^2}{2\alpha^2 \cosh^2 ah} \left( \frac{-1}{8\alpha^2} + \frac{h^2}{12} - \frac{\cosh 2ah}{8\alpha^2} + \frac{\sinh 2ah}{8h\alpha^3} \right) \quad [14]$$

**3.1 CASE 1:**

**Fluid flow in a medium with high porosity i.e flow for small values of  $\alpha$  or large values of the porosity coefficient  $k^*$**

Neglecting terms of  $\alpha$  higher than  $O(\alpha^2)$  we get

**Velocity:**  $u(y) = c_1 \left\{ \frac{(2hy - y^2)}{2} - \frac{\alpha^2}{24} (8h^3 y - 4hy^3 + y^4) \right\}$  [15]

**Mean velocity**  $\bar{u} = \frac{1}{h} \int_0^h u dy = \frac{c_1 h^2}{15} (5 - 2\alpha^2 h^2)$  [16]

**Temperature:**

$$\theta(y) = \frac{y}{h} + \frac{P_r c_1 c_2}{720} \left[ (120hy^3 - 90h^3 y - 30y^4) - \alpha^2 (h^6 - 36h^5 y + 40h^3 y^3 - 6hy^5 + y^6) \right] + \frac{Ec_1^2}{8640} \left[ 720(3h^3 y - 6h^2 y^2 + 4hy^3 - y^4) - \alpha^2 \left( 791h^6 - 576h^5 y + 2160h^4 y^2 + 960h^3 y^3 + 720h^2 y^4 - 576hy^5 + 96y^6 \right) \right] \quad [17]$$

**Mean temperature:**

$$\bar{\theta} = \frac{1}{h} \int_0^h \theta dy = \frac{1}{2} - \frac{P_r c_1 c_2 h^4}{5040} (147 + 575\alpha^2 h^2) + \frac{Ec_1^2 h^4}{210960} (5274 + 907\alpha^2 h^2) \quad [18]$$

**3.2 CASE 2. For large values of  $\alpha$  i.e for low porosity**

For large  $\alpha$   $\sinh ah \approx \frac{e^{ah}}{2}$  ;  $\cosh ah \approx \frac{e^{ah}}{2}$  ;  $\tanh ah \approx 1$  and neglecting the terms of

$O\left(\frac{1}{\alpha^3}\right)$  we get

**Velocity:**  $u(y) = \frac{c_1}{\alpha^2} (1 - e^{-\alpha y})$  [19]

**Mean velocity:**  $\bar{u} = \frac{c_1}{\alpha^2}$  [20]

**Temperature:**  $\theta(y) = \frac{y}{h} - \frac{P_r c_1 c_2 (h - y)y}{2\alpha^2}$  [21]

$$\text{Mean Temperature: } \bar{\theta} = \frac{1}{h} \int_0^h \theta dy = \frac{1}{2} - \frac{p c c h^2}{12 \alpha^2} \quad [22]$$

4. GRAPHICAL ILLUSTRATIONS

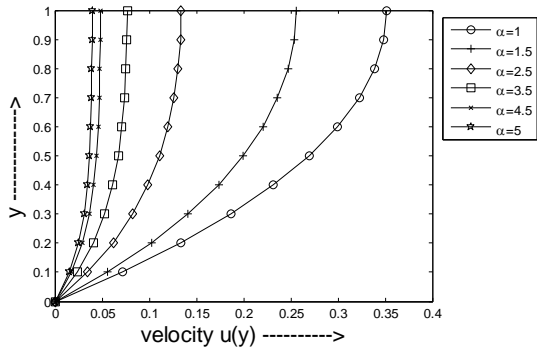


Fig.1 velocity profile for c1=1 and h=1

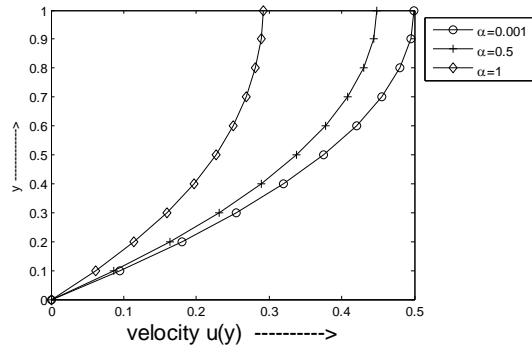


Fig.2. velocity profile for small alpha, c1=1 & h=1

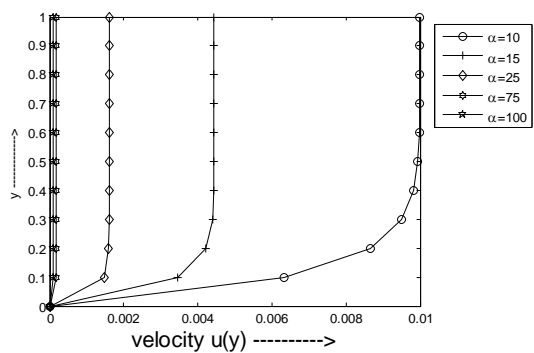


Fig.3. velocity profile for large alpha, c1=1 & h=1

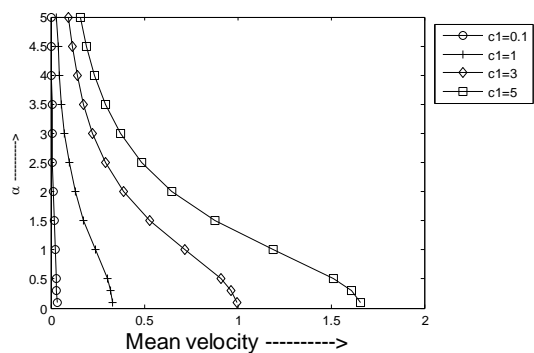


Fig.4 mean velocity for h=1

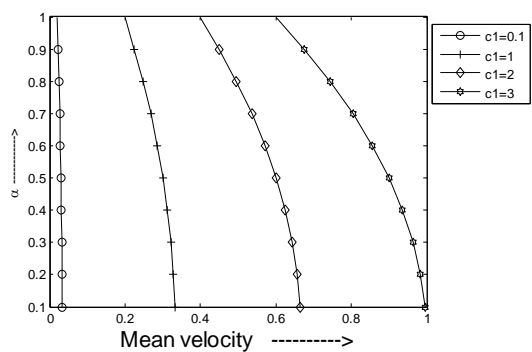


Fig.5. Mean velocity for small alpha & h=1

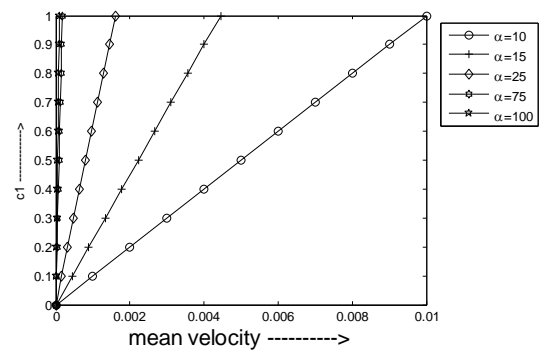


Fig.6. mean velocity for large alpha

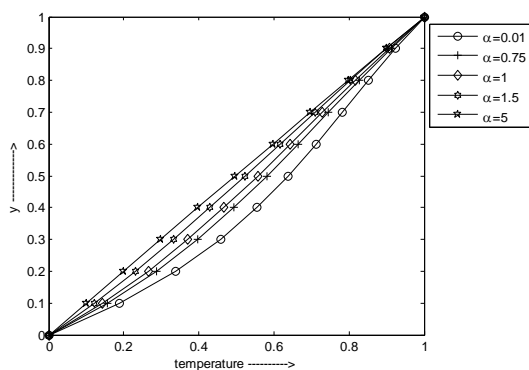


Fig.7. Temperature distribution for  $h=1, E=5, c_1=1, c_2=1, p=1$

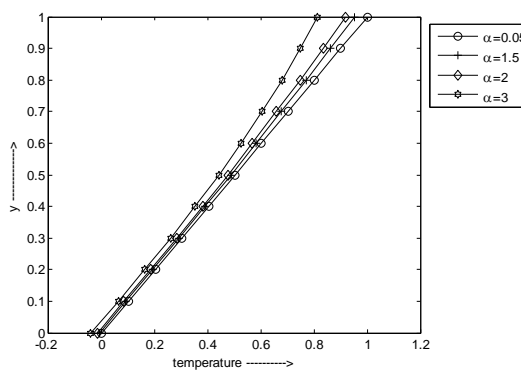


Fig.8. Temperature distribution for small  $\alpha$  & for  $h=1, E=5, c_1=1, c_2=5, p=1$

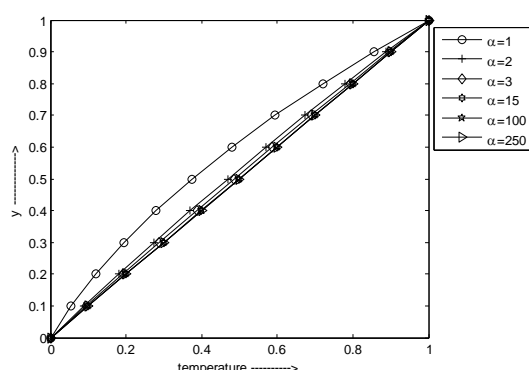


Fig.9. Temperature distribution for large  $\alpha$  & for  $h=1, E=5, c_1=1, c_2=1, p=1$

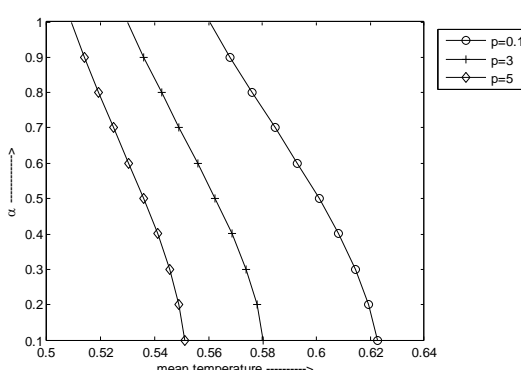


Fig.10. Mean Temperature for  $h=1, E=5, c_1=1, c_2=5$

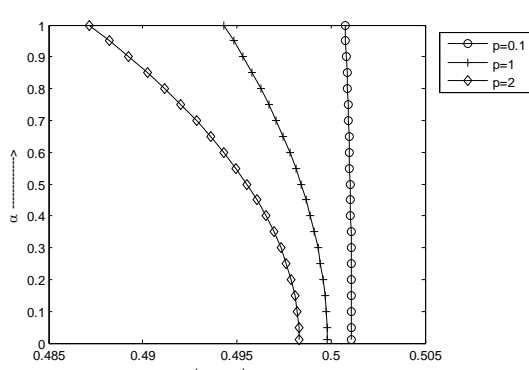


Fig.11. Mean Temperature for  $h=1, E=5, c_1=1, c_2=5$

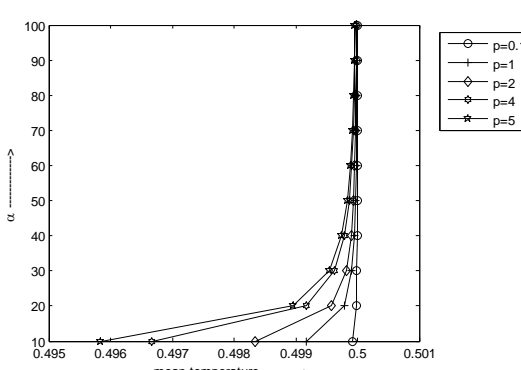


Fig.12. Mean temperature distribution for large  $\alpha$  & for  $h=1, E=5, c_1=1, c_2=1$

5. RESULTS AND DISCUSSIONS

It is noticed that the velocity profiles are more steep for large values of  $\alpha$  that is the velocity of the fluid decreases with the increase in the value of  $\alpha$  (Fig 1). From Fig.2, in the case of small  $\alpha$ , it is noticed that the velocity of the flow region decreases with the increase in the values of  $\alpha$ . For the case of large  $\alpha$ , Fig.3, illustrates that the velocity decreases with the increase in the values of  $\alpha$  and tends to zero for the values of  $\alpha$  bigger than 100.

It is evident from the Fig.4, that for the increasing values of the pressure gradient  $c_1$  the mean velocity increases and appears to be decreasing with the increase in the values of  $\alpha$ . Fig.5(for the case of small  $\alpha$ ), illustrates that the mean velocity is high for the higher values of the pressure gradient  $c_1$  at the bottom plate and decreases gradually with the increase in the values of  $\alpha$ . In the case of large  $\alpha$ , an increase in the values of  $\alpha$  decreases the mean velocity of the flow region ( Fig.6).

It is clearly illustrated in the Fig.7, that the temperature profiles gradually decreases with the increase in the values of  $\alpha$ . For the case of small  $\alpha$ , an increase in the value of  $\alpha$  decreases the temperature in the flow region(Fig.8). From Fig.9, in the case of large  $\alpha$ , it is noticed that the temperature profile

of the flow region increases with the increase in the values of  $\alpha$ , remains unaltered for large values of  $\alpha$ .

It is noticed that the mean temperature decreases as the prandtl number  $P$  increases along with the increase in the values of the porosity parameter  $\alpha$ . (Fig.10). In the case of small  $\alpha$ , Fig.11, illustrates that the mean temperature is high for smaller values of the prandtl numbers at the bottom plate and gradually decreases with the increase in the values of  $\alpha$ . Fig.12, in the case of large  $\alpha$ , illustrates that the mean temperature remains almost unaltered for higher values of  $\alpha$  and for lower values of  $\alpha$  it decreases with the increasing prandtl number  $p$ .

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