

method and integrated hydrological exploration of seismic exploration, Liu Shu-cai[11] etc improved the accuracy of coal mine water exploration; Based on the analysis of the combination of theory and experimental measurement, Ding Huan-de[12-13]studied the geological evolution law of coal measure strata, and revealed the characteristics of the geological environment of the special geological environment.

The aquifer is usually located above or below the coal seams, which rarely exists in the coal seams. Based on the special structure of "confined water storage in the No.2 main coal seam" in the Xiaojihan Coal Mine, this paper puts forward a new problem for the mine project [14].The mechanical properties of water bearing coal seams have great influence on the fracture production of coal seam[15], in relation to the production efficiency and safety of super large mine. However, the physical and mechanical properties of water bearing coal seams are different from that of conventional coal, which has special characteristics. In the paper, mechanical properties such as tensile strength and internal friction angle of water bearing coal are studied by the experiment[16-19], which provided some necessary basic data for the similar simulation and numerical simulation of the safety mining of the super large mine.

To summarize, prevention and control of water disasters and water conservation measures have a great significance in western coal mine. Yuheng Mining Area was a typical structure with shallow and thin loose sand strata-thick bedrock-coal seam bearing water. Based on the special geological conditions of Yuheng Mining Area, in this paper we analyzed geological conditions of coal seam as aquifer, and studied the mechanical characteristics of water bearing coal seam and explored the mechanism of mine water inrush.

2. MECHANICAL PERFORMANCE TEST OF XIAOJIHAN COAL SEAM

2.1. Sample and Test Plan

Collecting coal (rock) from Xiaojihan coal seam, according to the test procedure requirement for physical and mechanical properties of DY-94 rock, we processed sample as the core. The sample numbers are shown in Table 1.

Table1. *Sample size*

| Strata No. | Rock name | Sample number | Numbers (piece) | Diameter (mm) | Height (mm) | Thickness (mm) |
|------------|-------------------------------------------------|---------------|-----------------|---------------|-------------|----------------|
| 1 | Grain arkose in luohu group | C1 | 15 | 50 | 100 | 25 |
| 2 | Stable set of sandstone and mudstone interbed | C2 | 15 | 50 | 100 | 25 |
| 3 | Straight set of mudstone and sandstone interbed | C3 | 15 | 50 | 100 | 25 |
| 4 | Yanan group leader stone sandstone | C4 | 15 | 50 | 100 | 25 |
| 5 | Sandy mudstone yan'an group | C5 | 15 | 50 | 100 | 25 |
| 6 | Yanan leader Shi Shayan | C6 | 15 | 50 | 100 | 25 |
| 7 | Sandy mudstone yan'an group | C7 | 15 | 50 | 100 | 25 |
| 8 | No.2 coal | C8 | 15 | 50 | 100 | 25 |
| 9 | Rich county sandy mudstone | C9 | 15 | 50 | 100 | 25 |

The mechanical properties of typical strata of BS5 hole-drilling was tested, which includes uniaxial compression, triaxial compression and split test. Through uniaxial compression tests, we can get the rock uniaxial compressive strength, elastic modulus and ratio of Poisson. Through splitting test, we can get the tensile strength of rock. Through the three axis test; we can obtain the compressive strength and the internal friction angle of the four stage confining pressure.

2.2. Test Equipment and Principles

Uniaxial compression test, triaxial compression test and split test were carried out by the CMT5305 electronic universal machine, as shown in **Fig1**.

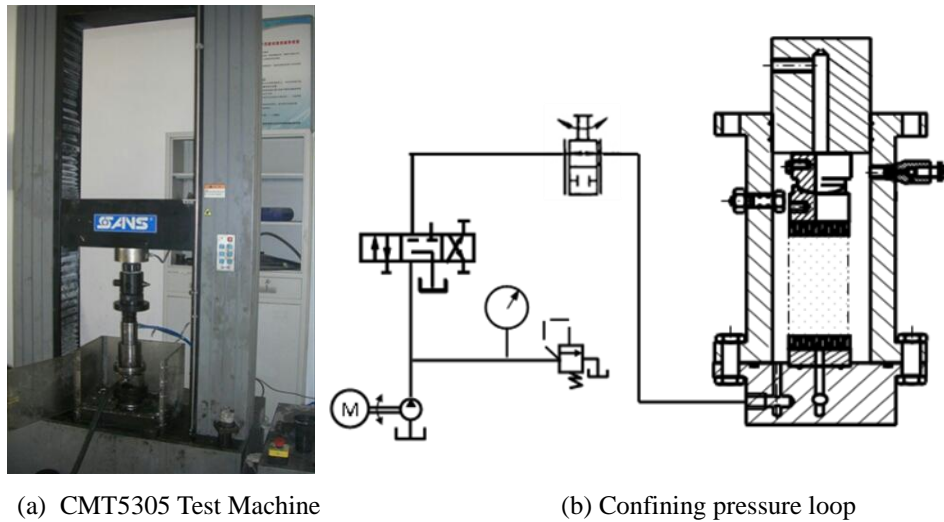


Fig1. Test system diagram

2.3. Uniaxial Compression Test

The uniaxial compression tests are shown as Fig 2. Measure the diameter for d_s and height for h_s of rock (coal) before the experiments. During the loading the system can collect the axial displacement u_a , axial load for p and radial displacement u_r . We can get the axial failure load p_b in the test data file and according to the following formula, we can calculate the uniaxial compressive strength of rock (coal) sample for σ_c .

$$\sigma_c = \frac{P_b}{\frac{\pi d_s^2}{4}} \quad (1)$$

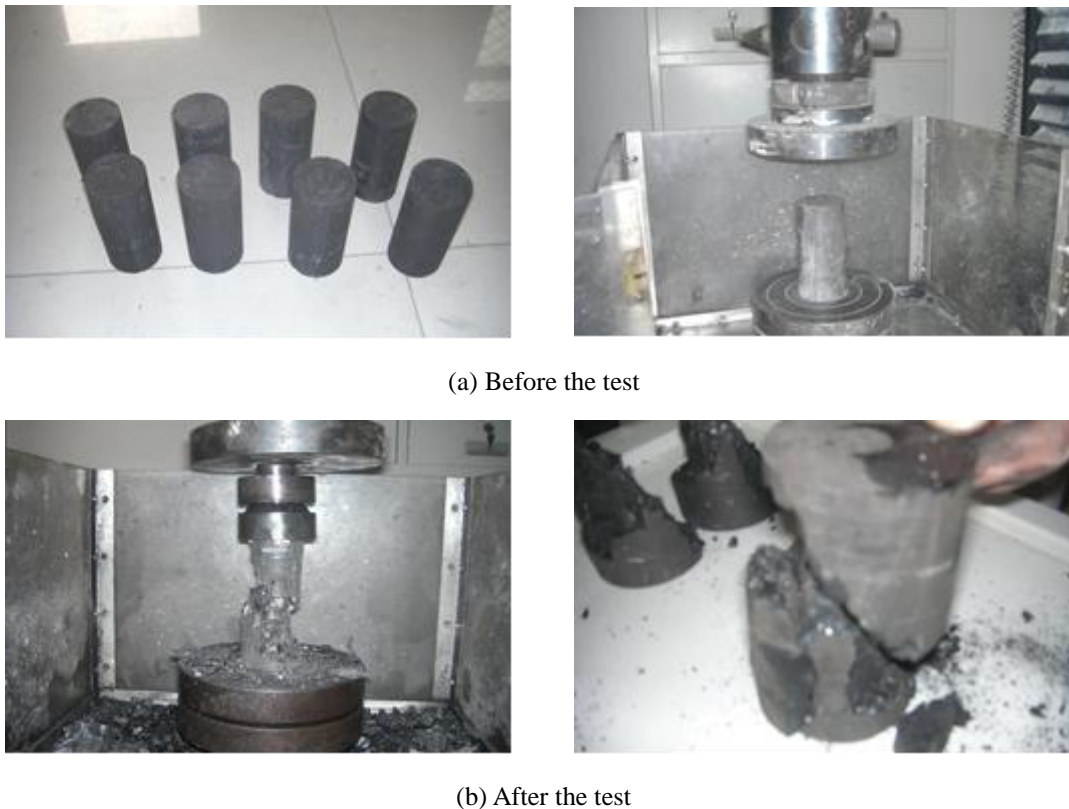


Fig2. Uniaxial compression test

For every moment, axial strain, circumferential strain and axial stress can be calculated by the formula $\varepsilon_\alpha = \frac{u_\alpha}{h}$, $\varepsilon_\theta = \frac{2u_r}{d_s}$, $\sigma_\alpha = \frac{P_b}{\frac{\pi d_s^2}{4}}$ respectively, so we can draw out the axial stress-strain curves and

circumferential strain-axial strain curves. The elastic modulus for E can be calculated by the straight line slope of the axial stress-strain curve, while Poisson's ratio can be calculated by the slope of the linear segment of the circumferential strain-axial strain curve.

2.4. Split Test

During the testing, the concentrated load is applied along the diameter direction of the cylindrical specimen; at last the specimen is cracked along the force direction. According to the elastic mechanics formula, the rock produced approximately horizontal uniform tensile stress along the direction perpendicular to force; the average value is as follows.

$$\sigma = \frac{2P}{\pi d_s h_s} \quad (2)$$

Where d_s is the core diameter, h_s is the rock height, P is the load. The tensile strength of rock is

$$\sigma_t = \frac{2P^*}{\pi d_s h_s} \quad (3)$$

Split test device is as shown in Fig 3.

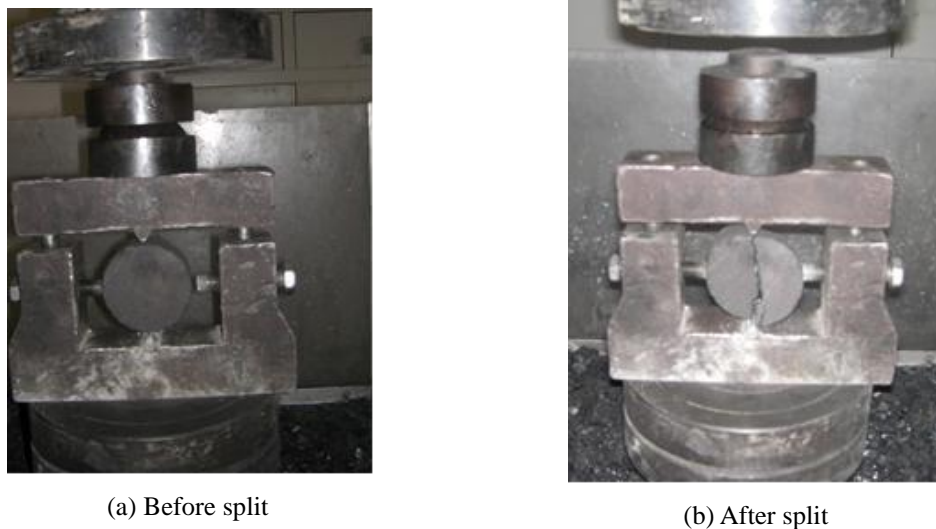


Fig3. Split test

2.5. Triaxial Compression Test

Triaxial compression test device is as shown in Fig 4.

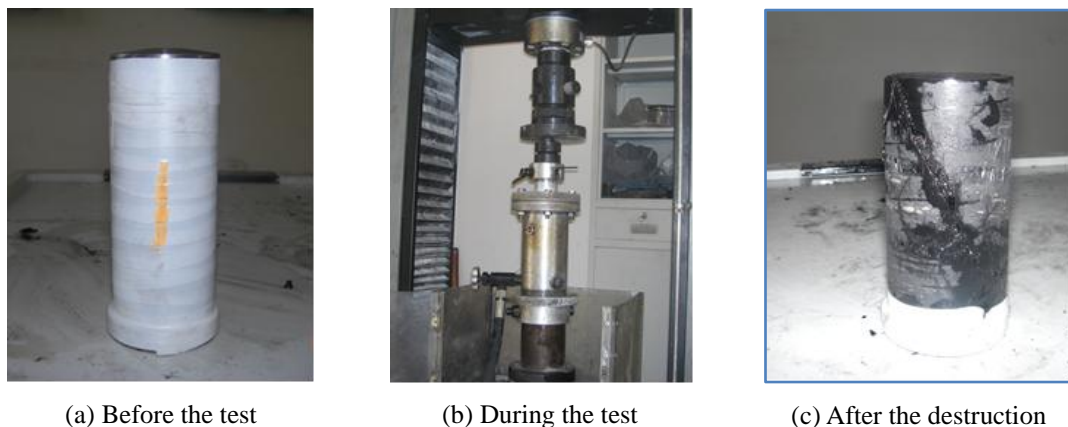


Fig4. Triaxial compression test

The diameter d_s and the height h_s were measured before the test. In test, we controlled the displacement velocity and load time and collected the axial displacement u_a and the axial load for P . Thus read axial

load P_b at failure in the test data file and based on equation (1), we can calculate the compressive strength of rock.

The broken rock obeys the Mohr-Coulomb criterion, when the failure occurs, the axial stress and confining pressure satisfied

$$\sigma_1 = \frac{2C \cos \phi}{1 - \sin \phi} + \sigma_3 \tan^2 \frac{\pi + \phi}{2} \tag{4}$$

Let $k_1 = \frac{2C \cos \phi}{1 - \sin \phi}$, $k_1 = \tan^2 \frac{\pi + \phi}{2}$, we can obtain $\sigma_1 = k + k_1 \sigma_3$ by the test results and linear regression, and then can calculate the internal friction angle for $\phi = 2 \arctan \sqrt{k_1} - \pi$ by k and k_1 .

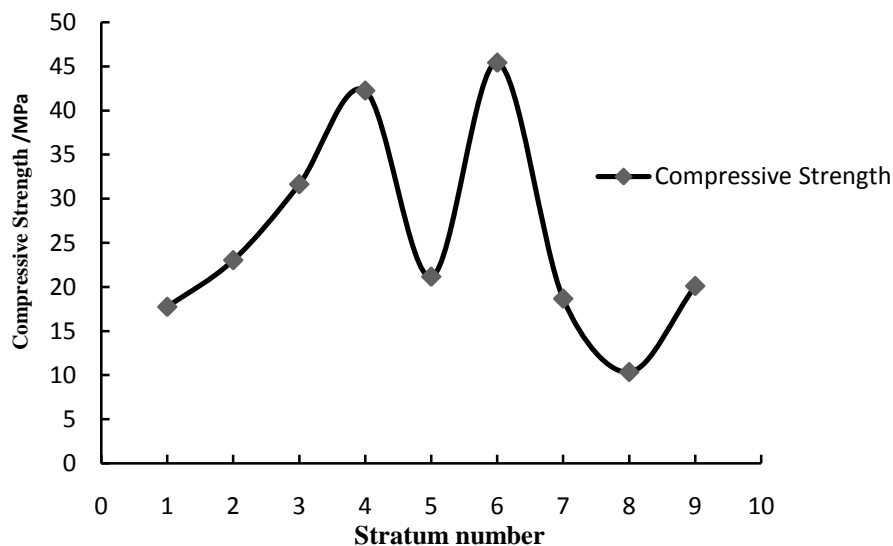
3. TEST RESULT

3.1. Compressive Strength

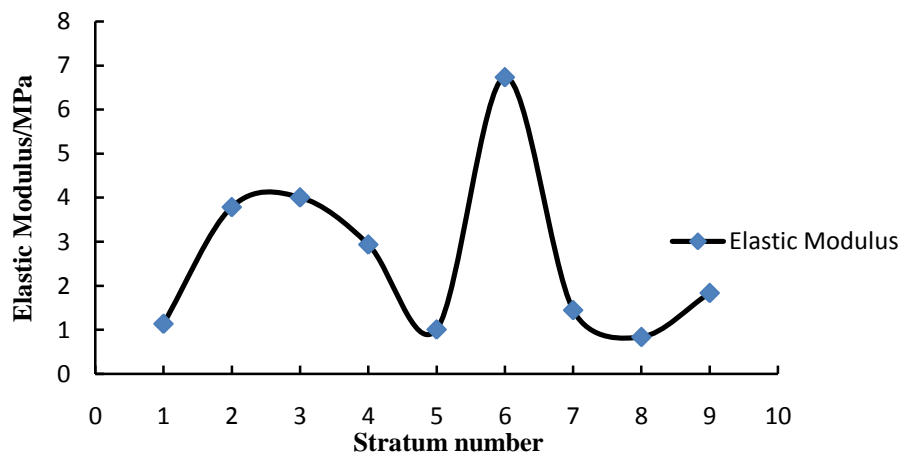
The uniaxial compression tests were carried out on the cylindrical rock sample with 100-mm-height and 50-mm-diameter from each stratum as shown in Table 1. These samples number from each stratum is 5. The compressive strength, elastic modulus and Poisson ratio of the specimens were obtained by tests. Results from an average of 5 groups are shown in Table 2. Comparison curves from uniaxial compression test results of different rock stratum are shown in Fig 5.

Table 2. Results of uniaxial compression test

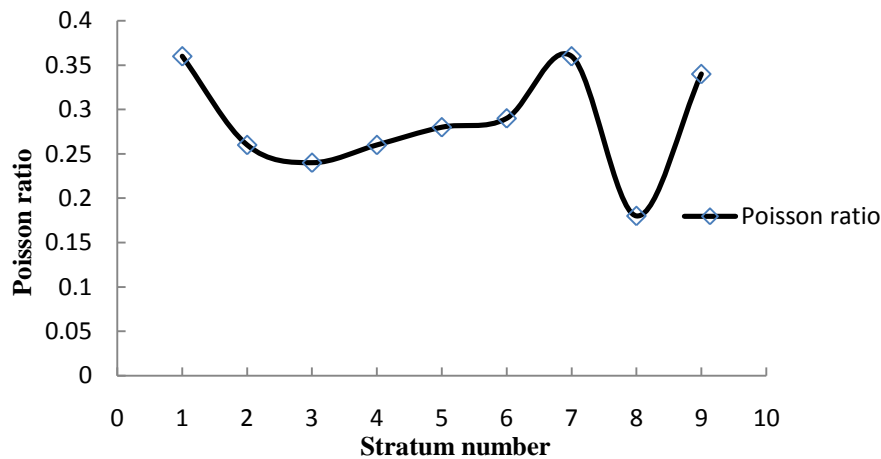
| Strata No. | Rock name | Diameter (mm) | Height (mm) | Elastic modulus (Gpa) | Poisson ratio | Compressive strength (MPa) |
|------------|-------------------------------------------------|---------------|-------------|-----------------------|---------------|----------------------------|
| 1 | Grain arkose in luohu group | 50 | 100 | 1.14 | 0.36 | 17.73 |
| 2 | Stable set of sandstone and mudstone interbed | 50 | 100 | 3.79 | 0.26 | 23.02 |
| 3 | Straight set of mudstone and sandstone interbed | 50 | 100 | 4.01 | 0.24 | 31.62 |
| 4 | Yanan group leader stone sandstone | 50 | 100 | 2.94 | 0.26 | 42.23 |
| 5 | Sandy mudstone yan'an group | 50 | 100 | 1.01 | 0.28 | 21.15 |
| 6 | Yanan leader Shi Shayan | 50 | 100 | 6.74 | 0.29 | 45.4 |
| 7 | Sandy mudstone yan'an group | 50 | 100 | 1.45 | 0.36 | 18.65 |
| 8 | No.2 coal | 50 | 100 | 0.84 | 0.18 | 10.34 |
| 9 | Rich county sandy mudstone | 50 | 100 | 1.84 | 0.34 | 20.09 |



(a) Compressive strength



(b) Elastic modulus



(c) Poisson ratio

Fig5. Comparison of uniaxial compression test results for different rock strata

3.2. Tensile Strength

The split tests were carried out on the circular-plate type rock sample with 25-mm-thick and 50-mm-diameter from each stratum as shown in Table 1. The samples number from each stratum is 5. The tensile strength of specimens was obtained by the average of 5 groups, as shown in Table 3. Comparison curves of tensile strength of different rock stratum are shown in Fig6.

Table3. Split test results

| Strata No. | Rock name | Diameter (mm) | Height (mm) | Tensile strength (MPa) |
|------------|-------------------------------------------------|---------------|-------------|------------------------|
| 1 | Grain arkose in luohu group | 50 | 25 | 1.62 |
| 2 | Stable set of sandstone and mudstone interbed | 50 | 25 | 2.11 |
| 3 | Straight set of mudstone and sandstone interbed | 50 | 25 | 3.03 |
| 4 | Yanan group leader stone sandstone | 50 | 25 | 4.18 |
| 5 | Sandy mudstone yan'an group | 50 | 25 | 2.26 |
| 6 | Yanan leader Shi Shayan | 50 | 25 | 4.31 |
| 7 | Sandy mudstone yan'an group | 50 | 25 | 1.83 |
| 8 | No.2 coal | 50 | 25 | 1.27 |
| 9 | Rich county sandy mudstone | 50 | 25 | 1.92 |

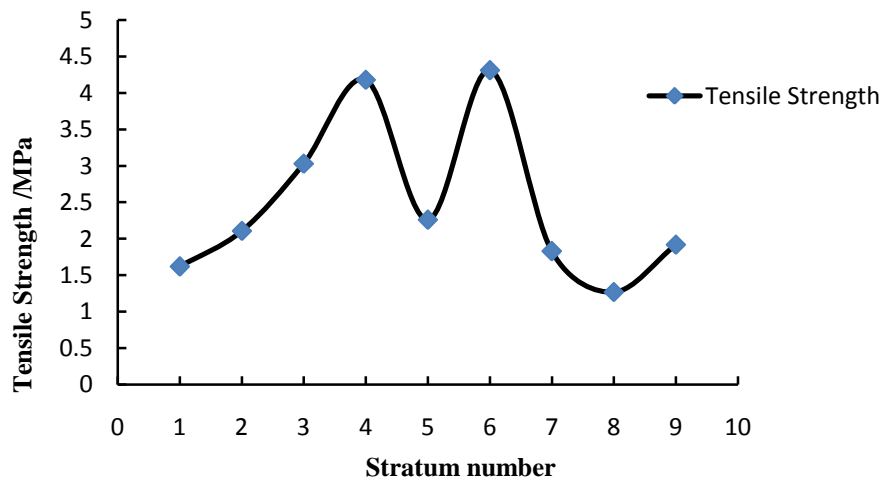


Fig6. Tensile strength curves of each stratum

Based on the research on the strength characteristics of water bearing coal seam(No.2),the compressive strength, elastic modulus, Poisson ratio (as shown in Fig. 5) and tensile strength (as shown in Fig. 6) are lower than that of the other strata, and its tension resistance ability is rather lower. This is the special physical and mechanical property which differs from the other rock stratum.

3.3. Internal Friction Angle

The confining pressure in triaxial compression test is set with five levels, which is divided into 0MPa, 2MPa, 4MPa, 6MPa and 8MPa respectively. The test results of the internal friction angle are shown in Table 4. Comparison curves of internal friction angle for different rock stratum are shown in Fig7.

Table4. Triaxial compression test results

| Strata No. | Rock name | Sample number | Diameter (mm) | Height (mm) | Confining pressure (MPa) | Compressive strength (MPa) | Internal friction angle (°) |
|------------|-------------------------------------------------|---------------|---------------|-------------|--------------------------|----------------------------|-----------------------------|
| 1 | Grain arkose in luohu group | C1-01 | 49.37 | 100.85 | 0 | 18 | 32.9 |
| | | C1-02 | 50.24 | 101.56 | 2 | 28.5 | |
| | | C1-03 | 50.82 | 99.97 | 4 | 34.5 | |
| | | C1-04 | 51.08 | 100.82 | 6 | 40.2 | |
| | | C1-05 | 49.8 | 101.31 | 8 | 46 | |
| 2 | Stable set of sandstone and mudstone interbed | C2-01 | 51.16 | 101.35 | 0 | 23.03 | 32.9 |
| | | C2-02 | 50.28 | 101.56 | 2 | 34.8 | |
| | | C2-03 | 50.72 | 100.87 | 4 | 40.2 | |
| | | C2-04 | 49.98 | 99.92 | 6 | 45.7 | |
| | | C2-05 | 49.29 | 101.41 | 8 | 51.3 | |
| 3 | Straight set of mudstone and sandstone interbed | C3-01 | 49.37 | 99.65 | 0 | 31.95 | 30.2 |
| | | C3-02 | 49.24 | 101.56 | 2 | 34.3 | |
| | | C3-03 | 50.52 | 99.87 | 4 | 41.5 | |
| | | C3-04 | 51.78 | 100.42 | 6 | 47.9 | |
| | | C3-05 | 51.89 | 101.41 | 8 | 55.4 | |
| 4 | Yanan group leader stone sandstone | C4-01 | 51.37 | 100.98 | 0 | 41.5 | 30 |
| | | C4-02 | 50.24 | 100.43 | 2 | 52.9 | |
| | | C4-03 | 49.52 | 99.87 | 4 | 57.6 | |
| | | C4-04 | 51.08 | 101.42 | 6 | 61.4 | |
| | | C4-05 | 49.89 | 99.81 | 8 | 67.3 | |
| 5 | Sandy mudstone yan'an group | C5-01 | 51.49 | 99.68 | 0 | 18.02 | 30.1 |
| | | C5-02 | 49.38 | 101.76 | 2 | 26.4 | |
| | | C5-03 | 50.83 | 100.39 | 4 | 31.5 | |
| | | C5-04 | 51.82 | 101.76 | 6 | 37.4 | |
| | | C5-05 | 50.76 | 99.28 | 8 | 42.6 | |

| | | | | | | | |
|---|----------------------------------|-------|-------|--------|---|-------|------|
| 6 | Yanan leader Shi Shayan | C6-01 | 51.24 | 99.12 | 0 | 46.2 | 30.2 |
| | | C6-02 | 49.78 | 101.38 | 2 | 53.4 | |
| | | C6-03 | 50.69 | 101.59 | 4 | 59.8 | |
| | | C6-04 | 51.01 | 99.46 | 6 | 65.2 | |
| | | C6-05 | 50.48 | 100.28 | 8 | 70.6 | |
| 7 | Sandy mudstone yanan group | C7-01 | 50.35 | 101.78 | 0 | 17.82 | 34.3 |
| | | C7-02 | 51.24 | 100.49 | 2 | 26.3 | |
| | | C7-03 | 49.92 | 99.79 | 4 | 35.9 | |
| | | C7-04 | 50.08 | 100.02 | 6 | 38.6 | |
| | | C7-05 | 49.81 | 99.87 | 8 | 47.5 | |
| 8 | No.2 coal | C8-01 | 51.23 | 100.68 | 0 | 8.89 | 24 |
| | | C8-02 | 49.88 | 101.43 | 2 | 9.2 | |
| | | C8-03 | 50.13 | 100.48 | 4 | 14.6 | |
| | | C8-04 | 50.81 | 100.74 | 6 | 19.8 | |
| | | C8-05 | 51.76 | 101.28 | 8 | 27.3 | |
| 9 | Rich county sandy mudstone | C9-01 | 51.04 | 99.66 | 0 | 19.6 | 35.1 |
| | | C9-02 | 49.78 | 100.31 | 2 | 28.6 | |
| | | C9-03 | 50.69 | 101.45 | 4 | 38.5 | |
| | | C9-04 | 49.91 | 100.46 | 6 | 42.6 | |
| | | C9-05 | 50.48 | 100.28 | 8 | 49.7 | |

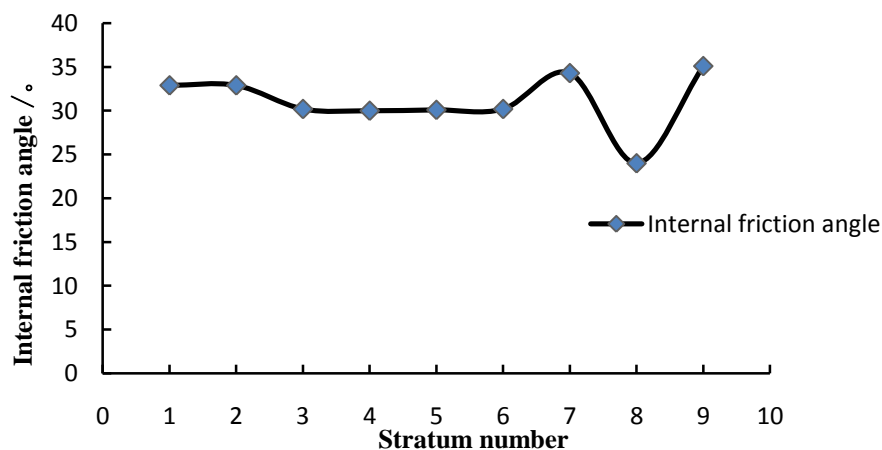


Fig7. Comparison of the internal friction angle for different rock layers

It can be seen from Fig7 that the internal friction angle of other strata is normal, while this angle of the No.2 coal seam is small, which explained that the fracture of the No.2 coal seam is not easy to close. The internal friction angle of the other adjacent rock stratum located at the up or down coal seam is large, so the fracture is easy to close; therefore, water in the No.2 coal seam streams (or flows) hard up and down. This is also an important reason for the No.2 coal seam is the main aquifer.

4. CONCLUSIONS

By CMT5305 Testing Machine, the experiments including uniaxial compression, split, triaxial compression were carried out to the rock (coal) sample from the Xiaojihan coal mine. As a result, we obtained some mechanical properties of the test rock from the coal seam being the main aquifer of Xiaojihan Coal Mine. Research shows:

- 1) Differing from the common rock seam, the special physical and mechanical characteristics of the water bearing coal seam (No.2) is that its compressive strength, modulus of elasticity, Poisson, tensile strength and internal friction angle were lower than that of the other rock strata. Compared with the geological and hydrological structure of coal seam, the mechanical properties are more suitable to describe the characteristics of No.2 coal seam as main aquifer.
- 2) An important reason for coal seam containing water is that the internal friction angle of coal seam, by contrast, is too small for its fracture to close easily.

3) By studying the mechanical properties such as tensile and internal friction angle of water bearing coal seam (No.2), a reliable theoretical basis can be provided for predicting the working face in coal mine and the mine discharge, for establishing an early warning system about water disaster in mine, for designing and optimizing the technology in tunneling and coal mining about the flood preventing and controlling.

REFERENCES

- [1] Y B Tang, LJ Zhai, Y J Fu, X F Ma, Q M Li, Z X Li, R Zhang, (2012) Classification of hydro-geological types of coal base planning in China, *Chinese Coal Geological Exploration*, 09:28-32+49.
- [2] X X Miao, A Wang, Y J Sun, L G Wang, H Pu, (2012) Research on basic theory of mining with water resources protection and its application to arid and semi-arid mining areas. *Chinese Journal of Rock Mechanics and Engineering*, 09:28-32+49.
- [3] X X Miao, X B Mao, Z W Sun, H Pu, (2005) Formation conditions of compound key strata in mining over layer strata and its discriminance. *Journal of China University of Mining and Technology*, 05:547-550.
- [4] X Z Wang, J L Xu, W B Zhu, (2014) Study on the influence of the characteristic of unconsolidated confined aquifer on its property of load transfer. *Journal of Mining and Safety Engineering*, 499-505.
- [5] H B Bai, X X Miao, (2009) Research progress and major problems of water preserved coal mining. *Journal of mining and safety*, 253-505.
- [6] H W Qian, (2015) Study on the Deformation Mechanism of Water-rich Coal Roadway of Xiaojihan Coal Mine". *China University of Mining and Technology*.
- [7] B M Liu, (2012) Study on the method of hydrogeological control and productivity potential assessment of coal seam gas exploitation. *China University of Mining and Technology (Beijing)*.
- [8] Y L Liu, (2014) Study on the Key Factors of Water Inrush during Mining under the Unconsolidated Confined Aquifer of Hydrogeology and Engineering Geology. *An Hui University of Science Mid Technology*.
- [9] H Z Shen, (2005) Study on the hydrogeological characteristics of the fourth aquifer in the SuNan mining area. *AnHui University of Science Mid Technology*.
- [10] Z W Zhang, Q Wu, E J Fu, Z L Fan, (2011) Coal seam roof and floor hydrogeology conditions evaluation of Pingshuo No.1 mine and measures of preventing water bursting. *Engineering Science in China*, 11:94-101.
- [11] S C Liu, (2008) Mechanism of water inrush from coal seam floor and continuous survey of fractured zones in coal seam floor. *China University of Mining and Technology*.
- [12] H D Ding, Z M Mao, Q He, (2014) the hydrogeologic feature of Yuheng coal and its influence on research of coal seam mining. *Mining Technology*, 03: 92-95.
- [13] H D Ding, R GAO, Q He, (2014) Research on Safe and Efficient Road way Excavation. Technology of main aquifer coal seam. *Mining research and development*, 03: 38-40+69.
- [14] L Zhu, (2007) Several Simple Methods of Observing Quantity of Water Gush. *Coal Technology*, 01:86-87.
- [15] S Tao, Y B Wang, D N Tang, H Xu, W He, Y Li, (2012) Pore and Fracture Systems and Their Contribution to the Permeability of Coal Reservoirs in Southern Qinshui Basin. *Geological Journal of China Universities*, 03:522-527.
- [16] J Xu, X F Xian, Y G Du, G Y Zhang, (1993) An Experimental Study on the Mechanical Property of the Gas-filled Coal. *Journal of Chong Qing University*, 05:42-47.
- [17] P Lu, Z W Sheng, G W Zhu, E C Fang, (2001) The Effective Stress and Mechanical Deformation and Damage Characteristics of Gas-filled Coal. *Journal of University of Science & Technology China*, 06: 55-62.
- [18] P D Sun, X X Xian, Y M Qian, (1999) Experimental study on the law of effective stress of coal. *Mining safety and environmental protection*, 02:16-18+49.
- [19] C H Zhang, (2010) Simulation Experiment on the Mechanical Characteristics during out Bursting Coal Seam Uncovered by Crosscut. *Anhui University of Science and Technology*.

AUTHORS' BIOGRAPHY



Jingna Guo, is currently studying for a master's degree at China University of Mining and Technology. Her main research topics are Seepage mechanics of rock mass.



Qiang Li, is a Lecturer works in China University of Mining and Technology. He received Bachelors, Masters and Ph.D. degrees in Engineering Mechanics from China University of Mining and Technology. His current research topics are Seepage mechanics of mining rock mass.



Shun-cai Li, is a Professor of Jiangsu Normal University. She received a bachelor's degree in engineering mechanics from Chongqing University in 1991, a master's degree and a doctoral degree in engineering mechanics from China University of Mining and Technology in 2000 and 2006 respectively. Her current research topics are Seepage mechanics of mining rock mass.

Citation: *Jingna Guo et al. (2017). Experimental Study on the Mechanical Properties of Coal Seam as a Main Aquifer of Xiaojihan Coal Mine, International Journal of Mining Science (IJMS), 3(4), pp.24-33, DOI: <http://dx.doi.org/10.20431/2454-9460.0304003>.*

Copyright: © 2017 Jingna Guo. This is an open-access article distributed under the terms of the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original author and source are credited